

Early warning simulation for coastal inundation vulnerability induced by wave overtopping

2nd International workshop on
waves, storm surges and coastal hazards

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Motivation/Background

- Artificially treated (with hardening structures) coastal line > 53%
- Most storm inundation occurred due to wave overtopping (WOT)
- Severe storm surge inundation issued in 2016 due to WOT
- To meet increasing necessity of EWS (weather, storm, surge, wave, inundation, beach erosion,...)
- No existing all mighty model encompassing tide, wave, storm, **WOT**, **overland flow**,... (even coupling of models)
- Appropriate numerical treating is required for mathematical singularity solutions occurred in front of upright (steep slope) dikes (wetting-drying schemes cannot be applied)

Methods

- Simulation of storm wave overtop inundations on coastal infrastructures is difficult but EurOtop can empirically provide overtopping volumes, Q
- Evaluating Q and assigning for artificial dikes (levees)
- Incorporating EurOtop into ADCIRC+SWAN
- EurOtop functions are fully embedded in a coupled tide+wave+surge, ADCIRC+SWAN (as ver 53)
- Real-time storm surge + WOT forecasting system
- EWS of WOT in 2018

Results and discussion

- Hindcasting 2016 WOT inundation
- Comparison wrt videos and flood mark survey
- Limitations of EurOtop and further researches

Concluding remarks

- ✓ WOT functions are embedded completely in ADCIRC v53
- ✓ Additional computational time is $\sim 3\%$ compared to ADCIRC+SWAN even 0.1 sec of Δt for Marine city, Busan simulation
 - EWS of WOT can be successfully applied in other cases
- ✓ EWS can be done at least 1 d earlier → enough to make dynamic EAP
- ✓ Further study on sensitivity of surface reduction factor should be done, considering real-situation

Related articles

ADCIRC workshop presentations, papers

Ocean Dynamics (2015) 65:617–646
DOI 10.1007/s10236-015-0820-3

An efficient early warning system for typhoon storm surge based on time-varying advisories by coupled ADCIRC and SWAN

Seung Won Suh · Hwa Young Lee · Hyeon Jeong Kim ·
Jason G. Fleming

Journal of Coastal Research

SI

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Coconut Creek, Florida

2016

Application of EurOtop to Improve Simulations of Coastal Inundations due to Wave Overtopping

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www.cerf-jcr.org

ABSTRACT

Lee, H.Y. and Suh, S.W., 2016. Application of EurOtop to improve simulations of coastal inundations due to wave overtopping. *In: Vila-Concejo, A.; Bruce, E.; Kennedy, D.M., and McCarroll, R.J. (eds.), Proceedings of the 14th International Coastal Symposium (Sydney, Australia). Journal of Coastal Research, Special Issue, No. 75, pp. 1377 – 1381. Coconut Creek (Florida), ISSN 0749-0208.*



Journal of Coastal Research	SI	85	***_***	Coconut Creek, Florida	2018
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Simulation of Wave Overtopping and Inundation over a Dike Caused by Typhoon Chaba at Marine City, Busan, Korea

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www.cerf-jcr.org

ABSTRACT



Suh, S.-W. and Kim, H.-J., 2018. Simulation of wave overtopping and inundation over a dike caused by Typhoon Chaba at Marine city, Busan, Korea. *In*: Shim, J.S.; Chun, I., and Lim, H.S. (eds.), *Proceedings from the International Coastal Symposium (ICS) 2018* (Busan, Republic of Korea). *Journal of Coastal Research*, Special Issue No. 85, pp. ***-***, Coconut Creek (Florida), ISSN 0749-0208.

Journal of Coastal Research	SI	85	***_***	Coconut Creek, Florida	2018
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Efficient Real-time Erosion Early Warning System and Artificial Sand Dune Breaching on Haeundae Beach, Korea

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Kunsan, Republic of Korea



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ABSTRACT

**Thank you
for your attention
and...**

Overtopping example in 2012 induced by typhoon Sanba



Marine city inundation due to wave overtopping

Marine city flooding in 2016

- ✓ Induced by wave overtopping during typhoon Chaba passing
- ✓ Videos taken by cable news, SNS(Twitter, Facebook ...), YouTube



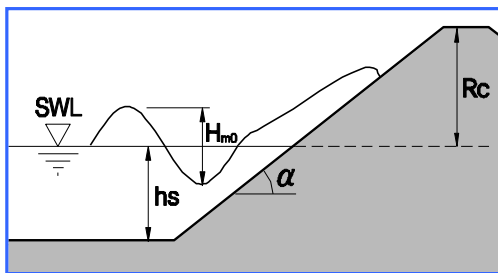
Marine city inundation videos

- Marine city flooding due to wave overtopping in 2016

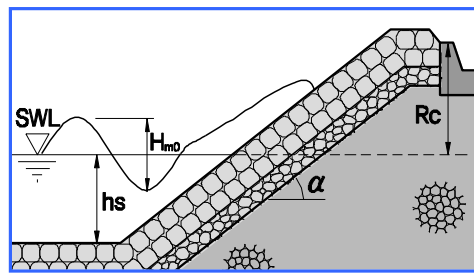


EurOTop overview

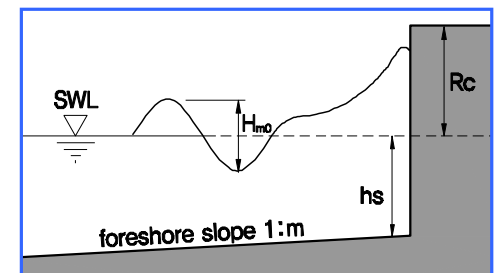
- **Integrated various wave overtopping formula taken**
 - HR Wallingford, Deltares, Infram ...
 - CLASH Project : experiment and Field data
 - Slope and vertical type structures
 - Probabilistic and deterministic design
 - Exponential (or Power) function type eq.
 - Effect of oblique waves, surface roughness type ...



Coastal Dikes & Embankment Seawalls



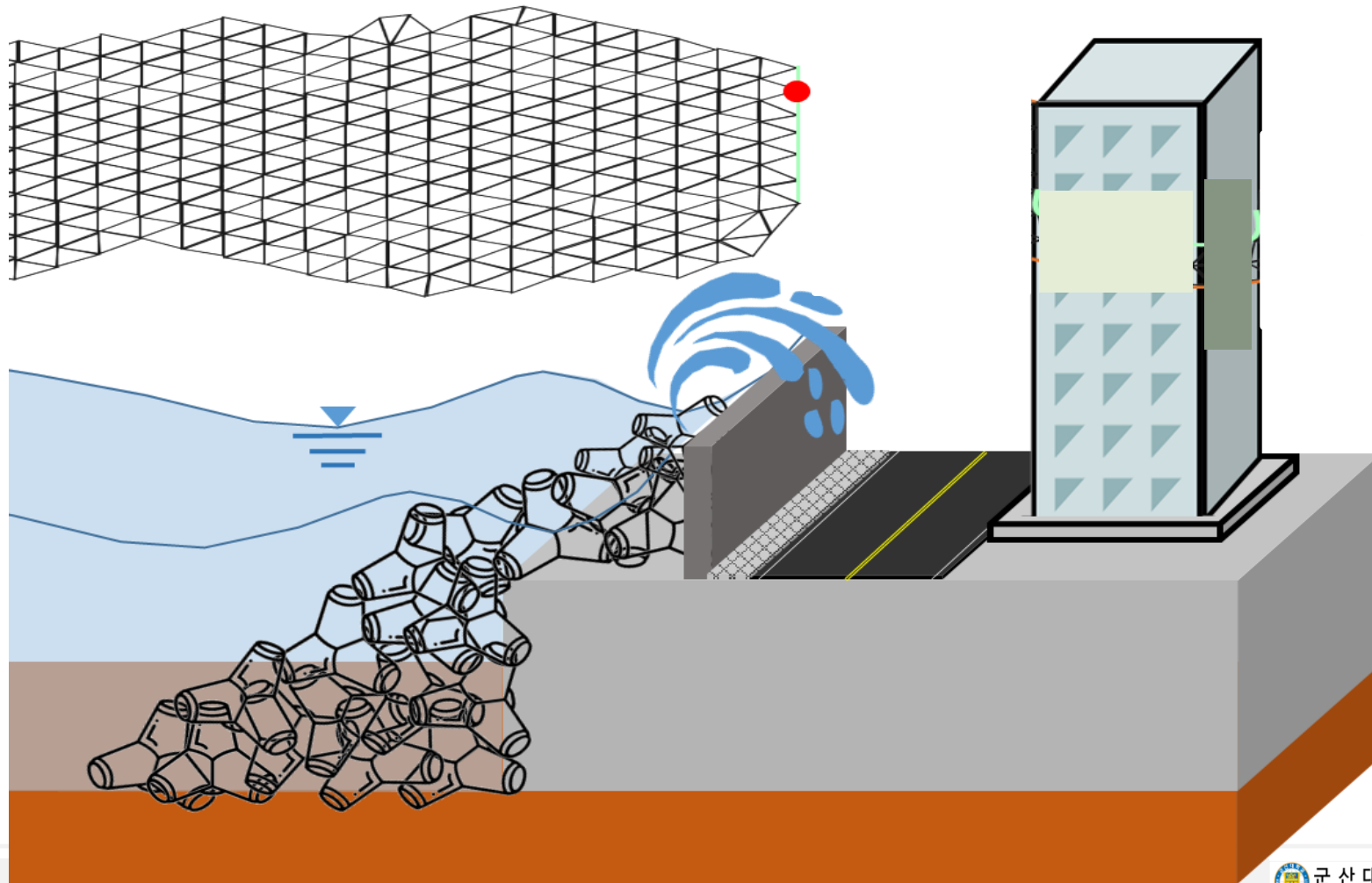
Armoured Rubble Slopes & Mounds



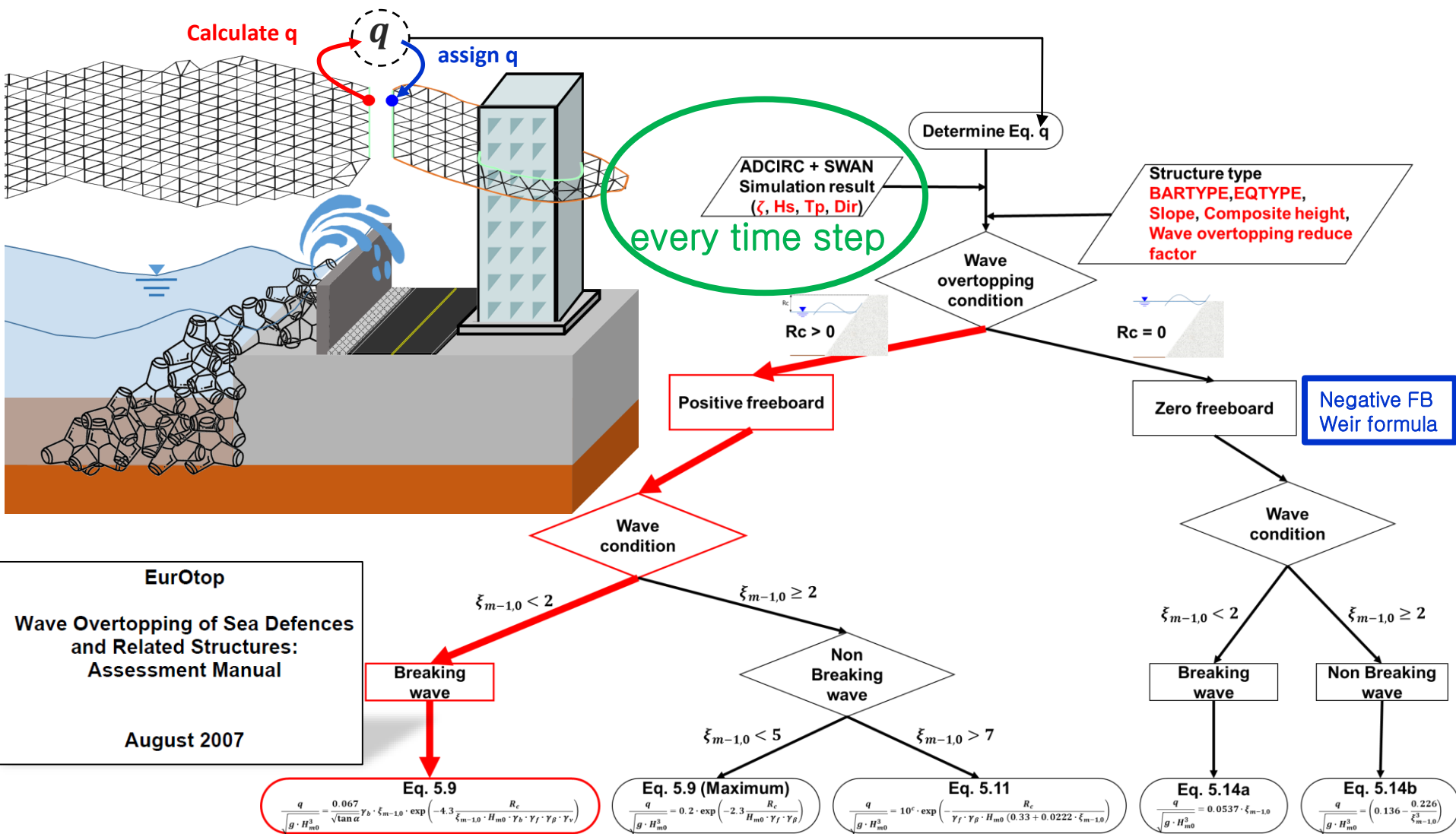
Vertical & Steep Seawalls

Calculation of WOT flow rates and conveying to landward

- Calculate wave overtopping volume for upright/steep slope dikes regardless of composite types, irregular surface canopy conditions



All procedures automatically performed



EurOtop
Wave Overtopping of Sea Defences
and Related Structures:
Assessment Manual
August 2007

Grid file (Fort.14)

Internal barrier type(24) segment

101 24 = Number of paring node for weir (land boundary 4)

NBVV	IBCONN	BARINHT	BARINCFSB	BARINCFSF
4434	2130	2.8	1.0	1.0
4432	2252	2.8	1.0	1.0
4431	2253	2.8	1.0	1.0
4430	2251	2.8	1.0	1.0

BARTYPE	EQTYPE	BSLOPE	BARHT	BARCF
1	1	1	0	1.0
1	1	1	0	0.3
3	2	2	0	0.3
3	2	2	0	0.3

Original barrier boundary setup element

NBVV : node numbers on normal flow boundary

IBCONN : back face node paired with the front face node

BARINHT : internal barrier height

BARINCFSB : coefficient of free surface subcritical flow at internal barrier node

BARINCFSF : coefficient of free surface supercritical flow at internal barrier node

Added structure type

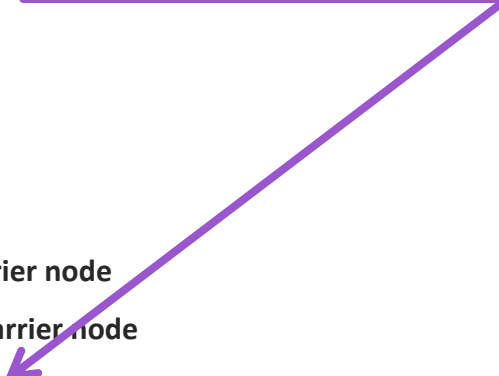
BARTYPE: Vertical wall=1, Simple sloped barrier=3

EQTYPE: Deterministic eq=1, Probabilistic eq=2 , Default=1

BSLOPE: Slope

BARHT: Composite height (m)

BARCF: Wave overtopping reduction factor



Control file (Fort.15)

```
1          ! NOLICAT - OPTION TO CONSIDER TIME DERIVATIVE OF CONV ACC TERMS
3          ! NWP - Number of nodal attributes.
primitive_weighting_in_continuity_equation
mannings_n_at_sea_floor
wave_refraction_in_swan
1          ! NCOR - VARIABLE CORIOLIS IN SPACE OPTION PARAMETER
1          ! NTIP - TIDAL POTENTIAL OPTION PARAMETER
319 1      ! NWS - WIND STRESS AND BAROMETRIC PRESSURE OPTION PARAMETER
1          ! NRAMP - RAMP FUNCTION OPTION
9.81       ! G - ACCELERATION DUE TO GRAVITY - DETERMINES UNITS
-3         ! TAU0 - WEIGHTING FACTOR IN GWCE
0.1        ! DT - TIME STEP (IN SECONDS)
0.0        ! STATIM - STARTING SIMULATION TIME IN DAYS
0.0        ! REFTIME - REFERENCE TIME (IN DAYS) FOR NODAL FACTORS AND EQUILIBRIUM ARGS
2016 10 02 00 1 0.7 600
10.375     ! RNDAY - TOTAL LENGTH OF SIMULATION (IN DAYS)
```

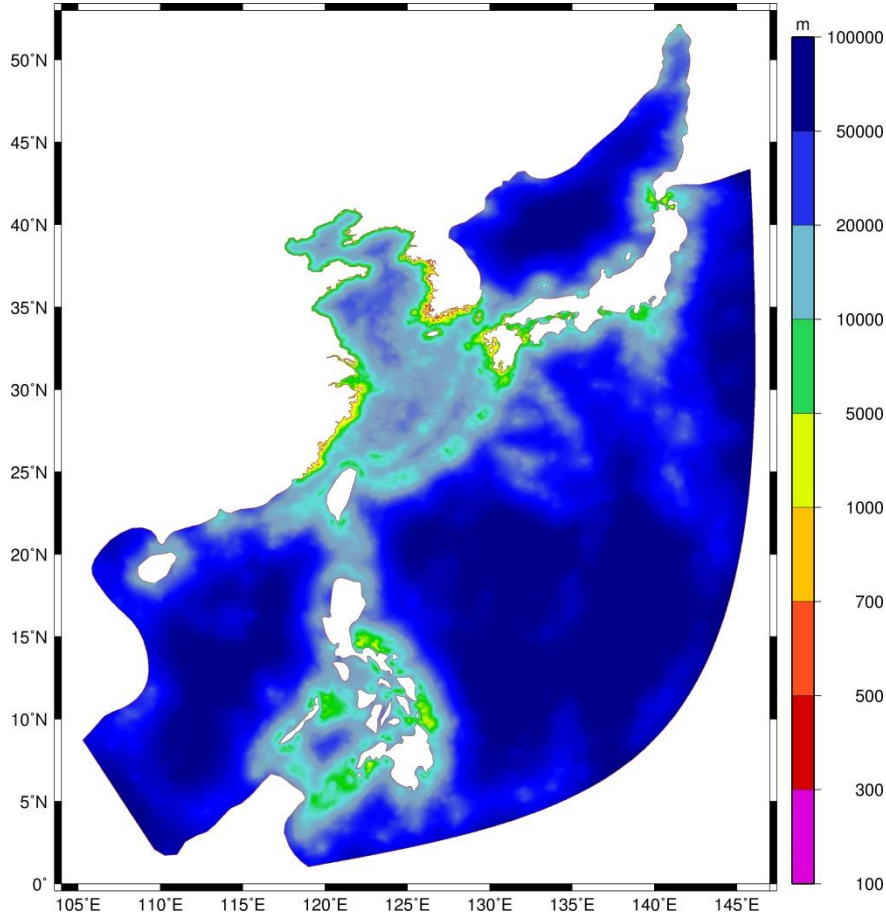

Source code (wot.f)

```
97 C      reduction factor considered due to incident wave angle (vertical dike)
98     W_Q=0.D0          ! mean overtopped volume m3/s/m
99     WBK=0.D0          ! wave breaking parameter(IRIBARREN NUMBER)
100    S0=0.D0           ! barrier slope (e.g. slope=1:2 then input 2)
101    W_H=0.D0          ! impulsiveness parameter h*
102    VALID_WO=0.D0     ! validity index of EurOtop Eqs application condition
103    R_C=0.D0          ! freeboard distance (crest level - swl) stilling water level
104    IN_WAVE_A2=0.D0   ! initial wave incident angle
105    DANG_A=0.D0
106    DANG_B=0.D0
107    DEP_CHK=0.D0      ! depth check for divergence problem in wet-dry area    DEP_
108    BAR_ANGLE=BAR_ANGLE1
109 C .... WOT is defined in fort.15 (0: no computation, 1: wave overtopping)
110 C.... needed next variables in fort.14
111 C.... BARTYPE: barrier (structure) type: VERTICAL WALL=1, SIMPLE SLOPED BARRIER=3
112 C          Incompleteness:(COMPOSITE VERTICAL WALL=2, COMPOSITE SLOPE BARRIER=4)
113 C .... EQTYPE: Type of computation; Deterministic EQ = 1 OR Probabilistic EQ = 2, default = 1
114 C.... SLOPE: Slope of the sloped dike (only valid for BARTYPE = 3)
115 C.... BARCF: Friction coeff of barrier such as reduction factor of tetra-pod
116 C          (only valid for sloped dike)
117 C.... READ_INPUT.F modified
118 C.... WAVE_H3   significant wave height (HS)
119 C.... WAVE_A3   mean wave DIRecton (DIR); NORTH=0 degree clockwise ==> only antic coupling
120 C.... WAVE_T3   mean wave periods(TM01)
121 C.... NNBB2: seaward barrier node number
122 C.... ETA2: SURFACE ELEVATION
123 C.... DP: water depth(fort.14)
124 C.... QN2: normal flux through barrier
125
126
```

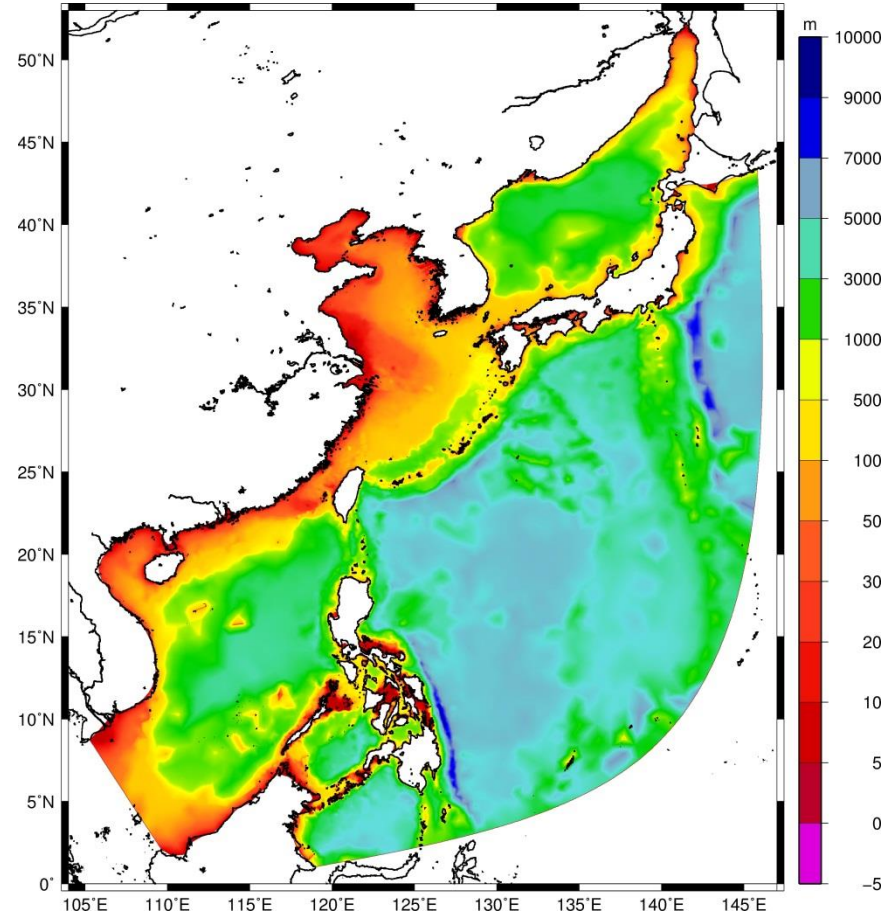
ADCIRC+SWAN+WOT compile (v53.00)

```
-rw-r--r-- 1 jung83kr team 7458 Mar 20 15:02 makefile.pc
drwxr-xr-x 2 jung83kr team 91 Mar 20 15:02 WOT_test
[jung83kr@oceansystem0 work]$ cd ./src
-bash: cd: ./src: No such file or directory
[jung83kr@oceansystem0 work]$ ll
total 188
-rw-r--r-- 1 jung83kr team 2847 Mar 20 15:36 actualflags.txt
-rw-r--r-- 1 jung83kr team 6620 Mar 20 15:02 adcirc_Xdmf.f
-rwxr-xr-x 1 jung83kr team 50875 Mar 20 15:02 cmplrflags.mk
-rwxr-xr-x 1 jung83kr team 44593 Mar 20 15:02 config.guess
-rwxr-xr-x 1 jung83kr team 34511 Mar 20 15:02 makefile
-rw-r--r-- 1 jung83kr team 5266 Mar 20 15:02 makefile_adcirc_dp.pc
-rw-r--r-- 1 jung83kr team 5266 Mar 20 15:02 makefile_adcirc_sp.pc
-rw-r--r-- 1 jung83kr team 3291 Mar 20 15:02 makefile_adcprep.pc
-rw-r--r-- 1 jung83kr team 13025 Mar 20 15:02 makefile.non_pc
-rw-r--r-- 1 jung83kr team 7458 Mar 20 15:02 makefile.pc
drwxr-xr-x 2 jung83kr team 91 Mar 20 15:02 WOT_test
[jung83kr@oceansystem0 work]$ make clean
makefile:19: (INFO) Guessing the type of platform ADCIRC will run on...
makefile:31: (INFO) Name is x86_64-unknown-linux-gnu, Machine is x86_64, Vendor is unknown, and OS is linux-gnu.
makefile:32: (INFO) The root directory for the build is /st2/jung83kr/ADCIRC/ADCIRC_53_WOT_v5
cmplrflags.mk:256: (INFO) Corresponding machine found in cmplrflags.mk.
makefile:38: (INFO) The compiler variable in cmplrflags.mk is set to intel-WOT.
makefile:40: (INFO) The following compilers have been selected...
makefile:41: (INFO) The Fortran compiler for adcprep is set to ifort.
makefile:42: (INFO) The serial Fortran compiler is set to ifort.
makefile:43: (INFO) The parallel Fortran compiler is set to mpif90.
makefile:44: (INFO) The C compiler is set to icc.
rm -f odir/**/*.o odir/**/*.mod sizes.o
rm -f ../swan/*.f ../swan/*.for ../swan/*.f90
[jung83kr@oceansystem0 work]$ ll
total 188
-rw-r--r-- 1 jung83kr team 2847 Mar 20 15:36 actualflags.txt
-rw-r--r-- 1 jung83kr team 6620 Mar 20 15:02 adcirc_Xdmf.f
-rwxr-xr-x 1 jung83kr team 50875 Mar 20 15:02 cmplrflags.mk
-rwxr-xr-x 1 jung83kr team 44593 Mar 20 15:02 config.guess
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-rw-r--r-- 1 jung83kr team 5266 Mar 20 15:02 makefile_adcirc_dp.pc
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-rw-r--r-- 1 jung83kr team 3291 Mar 20 15:02 makefile_adcprep.pc
-rw-r--r-- 1 jung83kr team 13025 Mar 20 15:02 makefile.non_pc
-rw-r--r-- 1 jung83kr team 7458 Mar 20 15:02 makefile.pc
drwxr-xr-x 2 jung83kr team 91 Mar 20 15:02 WOT_test
[jung83kr@oceansystem0 work]$
```

Real-time tide, wave, storm surge forecasting

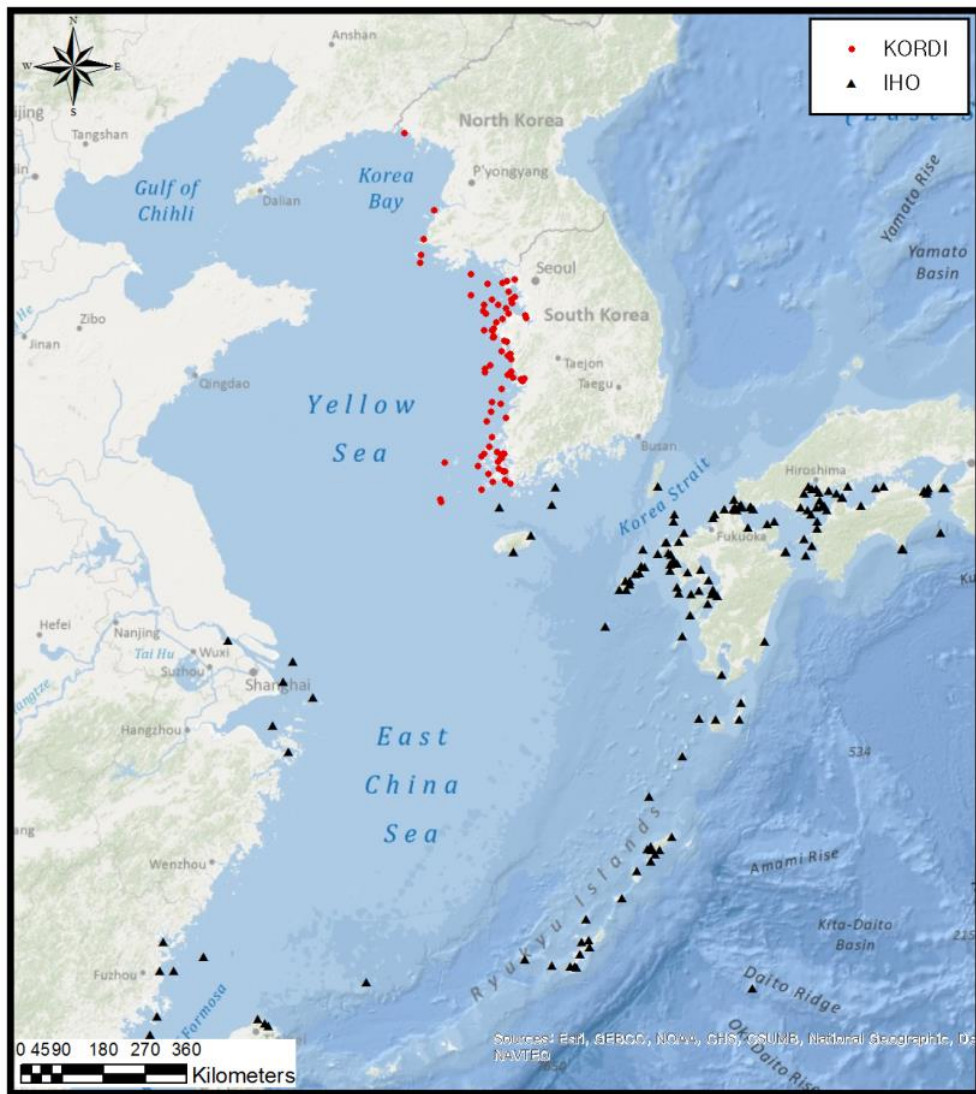


Basic grid structure(NWP-G57k)

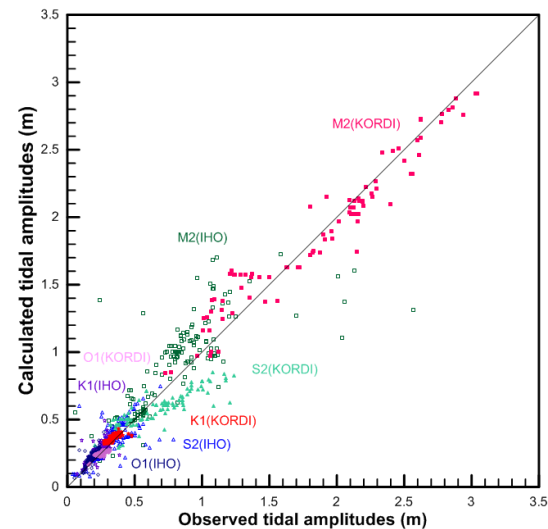


Bathymetry

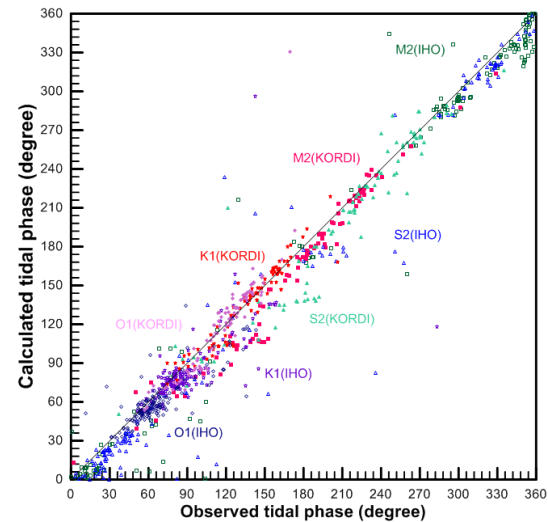
Tide simulation and verification



Stations (KORDI) : 96, (IHO) : 153



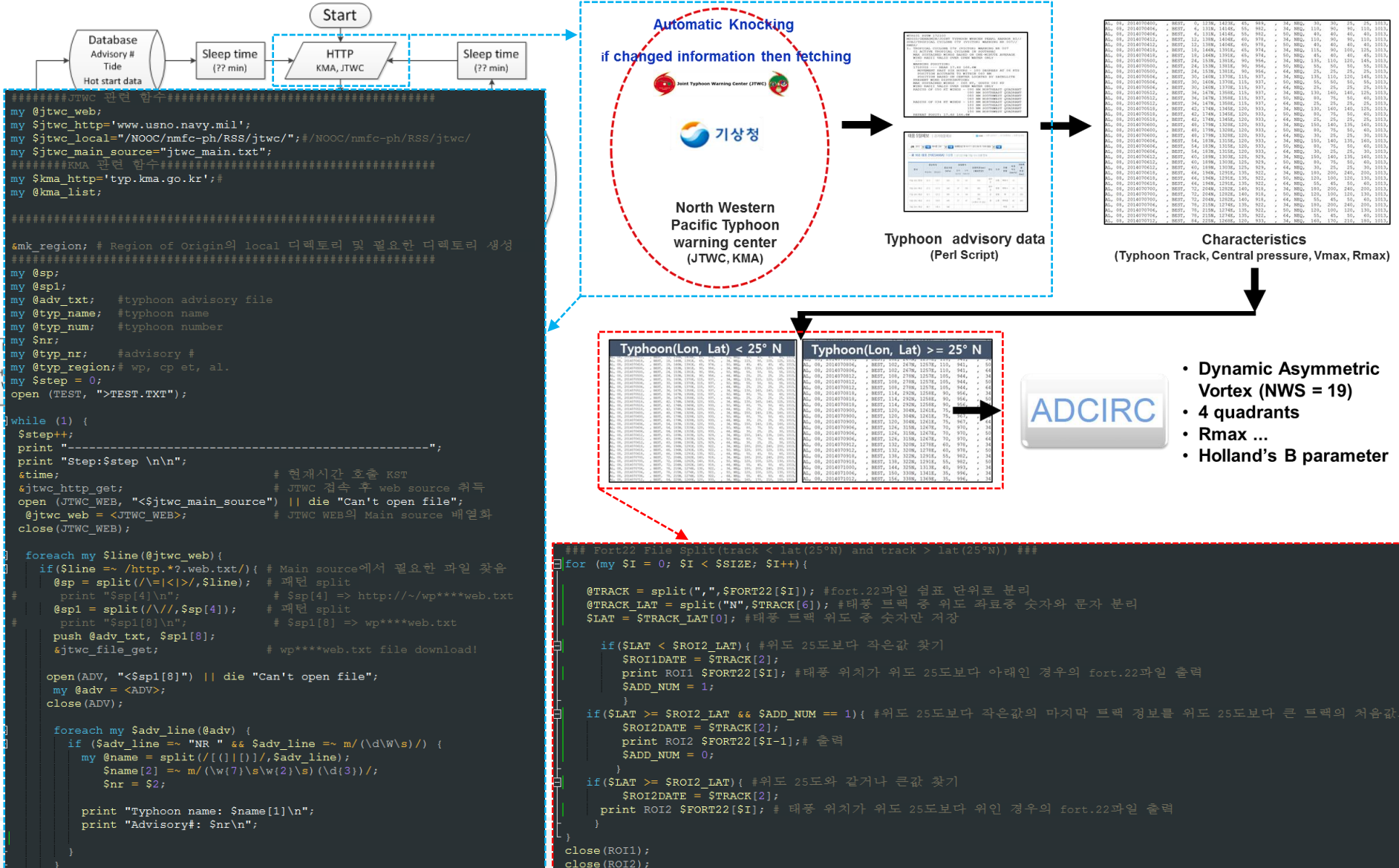
Amplitude - RMS : 0.138 m



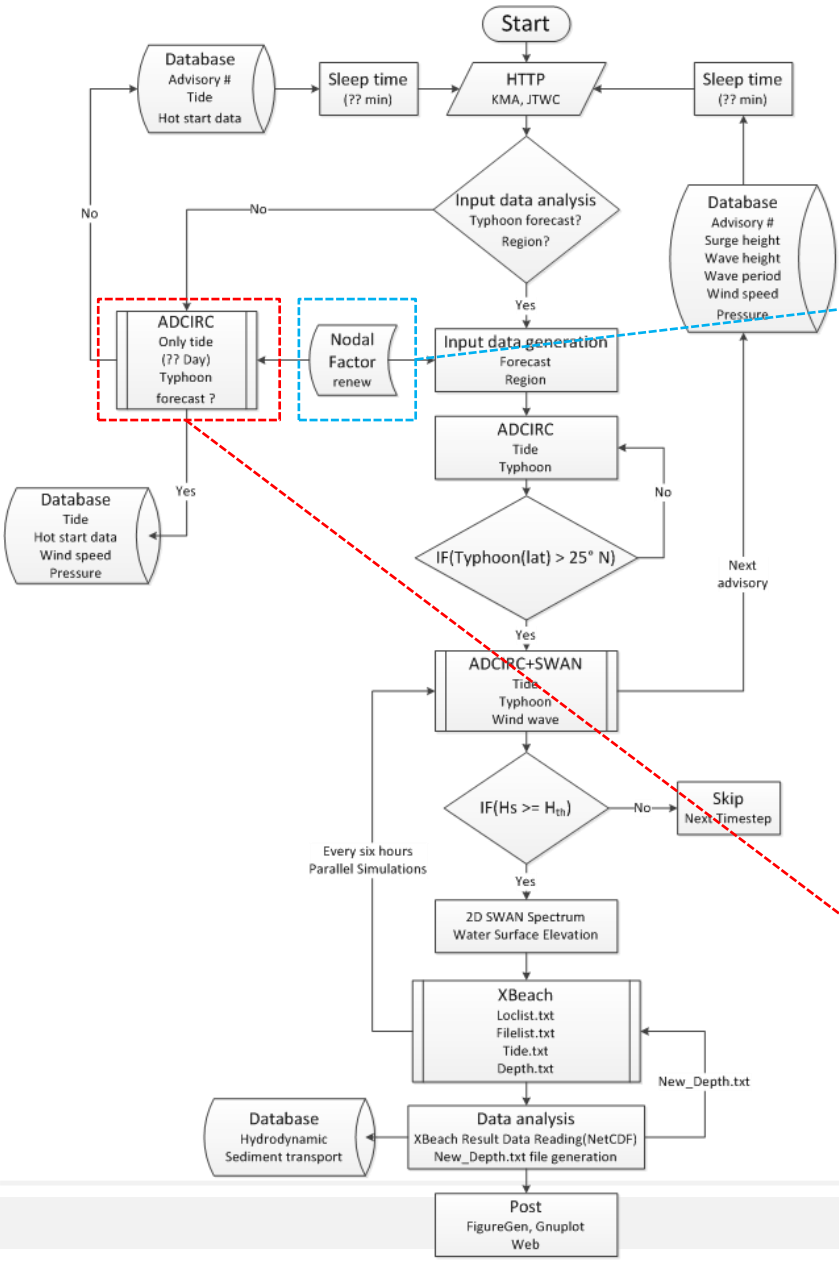
Phase - RMS : 20.53 deg

Automatic storm data fetching

Fetching Typhoon parameters and automatic input file creation



Automatic input file preparation



```

### ADCIRC Run(Tide) ###
system ("SEX_DIR/tide_fac.x --length $TIDEFAC LENGTH --year $CYEAR --month $CMONTH --day $CDAY --hour $CHOUR --outputformat
# TIDEFAC.x를 이용하여 시간설정 후 8분조의 진폭 및 위상 추출
unless (open (TIDEFAC,"<SEX_DIR/tide_fac.out")) {
die;
}

while(<TIDEFAC>) { # 8분조(M2, S2, N2, K2, K1, O1, P1, Q1)의 위상 및 진폭 변수화
my @constituent = split;
if ( $constituent[0] eq "M2" ) {
$M2nf = $constituent[1];
$M2eqarg = $constituent[2];
}
elseif ( $constituent[0] eq "S2" ) {
$S2nf = $constituent[1];
$S2eqarg = $constituent[2];
}
elseif ( $constituent[0] eq "N2" ) {
$N2nf = $constituent[1];
$N2eqarg = $constituent[2];
}
elseif ( $constituent[0] eq "K2" ) {
$K2nf = $constituent[1];
$K2eqarg = $constituent[2];
}
elseif ( $constituent[0] eq "K1" ) {
$K1nf = $constituent[1];
$K1eqarg = $constituent[2];
}
elseif ( $constituent[0] eq "O1" ) {
$O1nf = $constituent[1];
$O1eqarg = $constituent[2];
}
elseif ( $constituent[0] eq "P1" ) {
$P1nf = $constituent[1];
$P1eqarg = $constituent[2];
}
elseif ( $constituent[0] eq "Q1" ) {
$Q1nf = $constituent[1];
$Q1eqarg = $constituent[2];
}
} else {
stderrMessage("WARNING","Tidal constituent named '$constituent[0]' was unrecognized.");
}
}

close (TIDEFAC);
    
```

fort.15

```

unless (open (TYPHOON,"<fort_cold_temp.15") ) { # Fort.15 template파일 open
stderrMessage("ERROR","Failed to open the fort.15 template file fort_cold_temp.15 for reading.");
die;
}

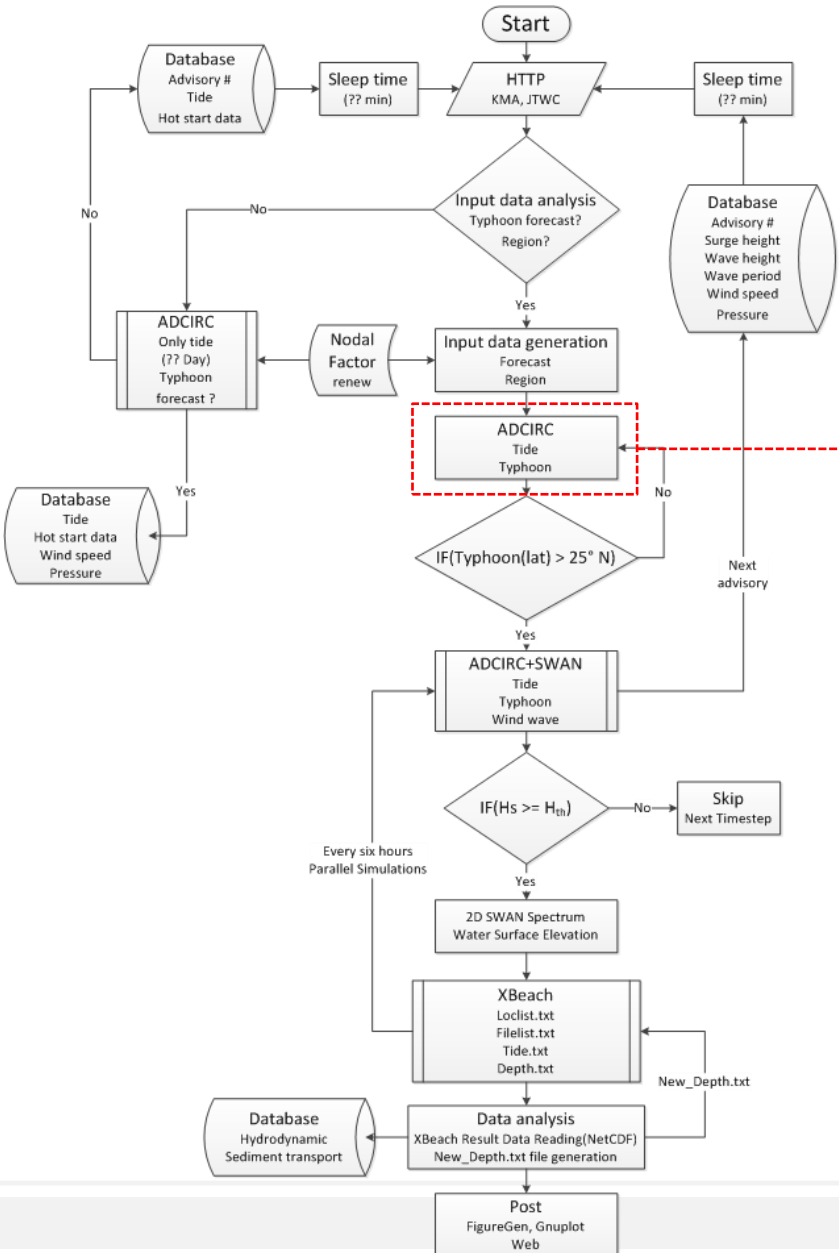
unless (open (TYPHOONR,">$SEX_DIR/fort.15") ) { # 아래의 내용을 적용할 파일
stderrMessage("ERROR","Failed to open the output control file $SEX_DIR/fort.15.");
die;
}

while(<TYPHOON>) { # 앞에서 설정한 8분조의 위상 및 진폭 적용, 모델 runtime 적용
s/%CRNDAY%/SCRNDAY/; # model run time
s/%M2NF%/Sm2nf/; # 8분조의 위상 및 진폭 적용
s/%S2NF%/Ss2nf/;
s/%N2NF%/Sn2nf/;
s/%K2NF%/Sk2nf/;
s/%K1NF%/Sk1nf/;
s/%O1NF%/So1nf/;
s/%P1NF%/Sp1nf/;
s/%Q1NF%/Sq1nf/;
s/%M2EQARG%/Sm2eqarg/;
s/%S2EQARG%/Ss2eqarg/;
s/%N2EQARG%/Sn2eqarg/;
s/%K2EQARG%/Sk2eqarg/;
s/%K1EQARG%/Sk1eqarg/;
s/%O1EQARG%/So1eqarg/;
s/%P1EQARG%/Sp1eqarg/;
s/%Q1EQARG%/Sq1eqarg/;
s/%CHOTSTARTFILE%/SCNHSTAR/;
unless (/NO LINE HERE/) {
print TYPHOONR $_;
}
}

close (TYPHOON);
close (TYPHOONR);
# 격자 분할 및 모델 run
system ("ADCIRC/adcprep --np $PROC --partmesh");
system ("ADCIRC/adcprep --np $PROC --parallel");
system ("time mpirun -machinefile ~/mpirun.hosts -np $PROC ADCIRC/padcirc");
sleep(1);
    
```

fort.15

Automatic storm surge modeling



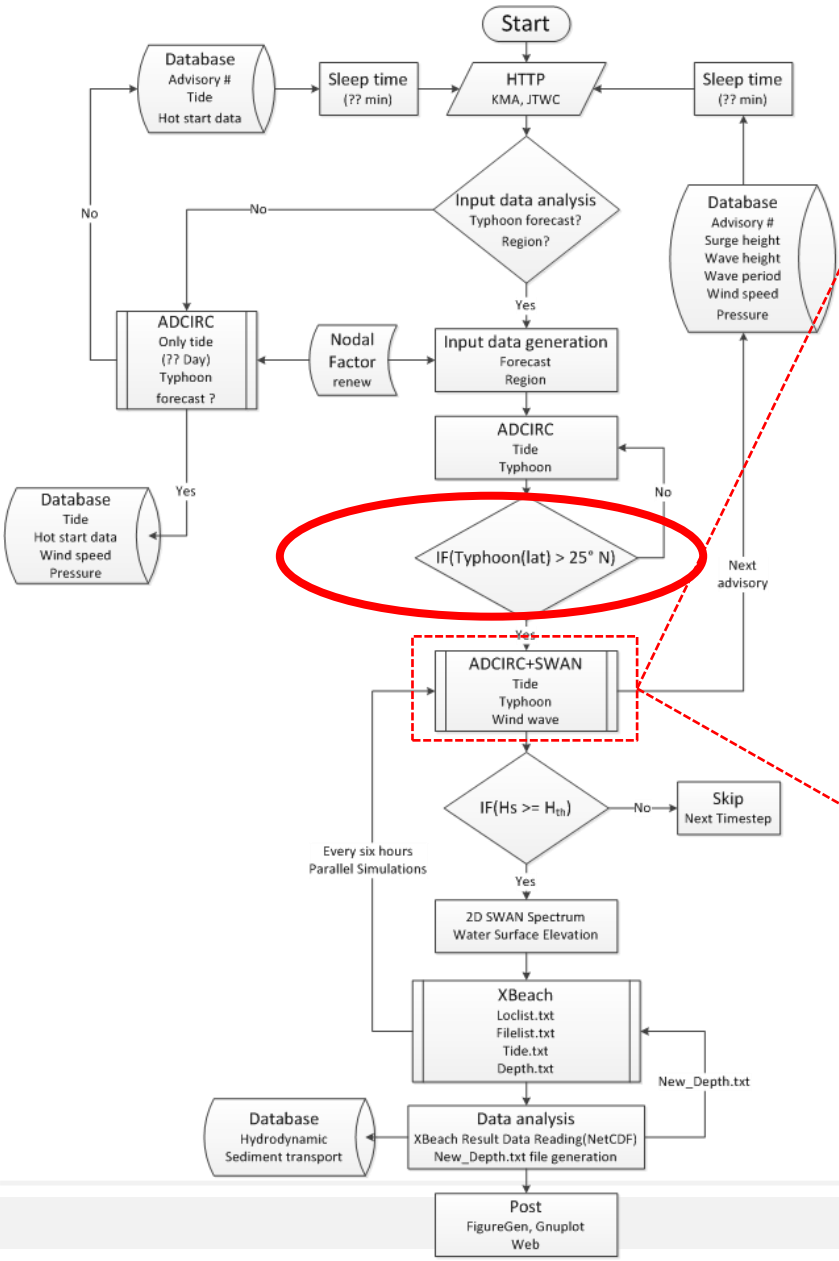
```

### ADCIRC Run(11111 Typhoon) ###
unless (open(TYPHOON1,"<fort_hot_temp.15") { # Fort.15 template file open
  stderrMessage("ERROR","Failed to open the fort.15 template file fort_hot_temp.15 for reading.");
  die;
}
unless (open(TYPHOONR1,">SEX_DIR/fort.15") { # 아래의 내용을 적용할 파일
  stderrMessage("ERROR","Failed to open the output control file SEX_DIR/fort.15.");
  die;
}
while(<TYPHOON1>) { # Tide 모의결과를 가지고 Tide + Typhoon모의(핫스타트), 모델 runtime 적용
  s/%IHOT%/SIHOT67; # hot-start파일 번호
  s/%HRNDAY%/SROI1RNDAY; # model run time
  s/%NWS%/SNWS_WOS; # 바람장 옵션 번호 (NWS=19)
  s/%REFTIME%/SCRNDAY; # 모델 runtime 적용
  s/%IREFYR%/SEYEAR; # 바람장 적용시간 (년)
  s/%IREFMO%/SEMONTH; # 바람장 적용시간 (월)
  s/%IREFDAY%/SEDAY; # 바람장 적용시간 (일)
  s/%IREFHR%/SEHOUR; # 바람장 적용시간 (시)
  s/%StormNumber%/SStormNumber; # 태풍번호
  s/%BLAdj%/SBLAdj;
  s/%HOTSTARTFILE%/SROI2HSTAR; # hot-start파일생성 간격
  s/%M2NF%/Sm2nf; # 8분조의 위상 및 진폭 적용
  s/%S2NF%/Ss2nf;
  s/%N2NF%/Sn2nf;
  s/%K2NF%/Sk2nf;
  s/%L2NF%/Sl2nf;
  s/%O1NF%/Solnf;
  s/%P1NF%/Sp1nf;
  s/%Q1NF%/Sq1nf;
  s/%M2EQARG%/Sm2eqarg;
  s/%S2EQARG%/Ss2eqarg;
  s/%N2EQARG%/Sn2eqarg;
  s/%K2EQARG%/Sk2eqarg;
  s/%L2EQARG%/Sl2eqarg;
  s/%O1EQARG%/Sol1eqarg;
  s/%P1EQARG%/Sp1eqarg;
  s/%Q1EQARG%/Sq1eqarg;
  unless (/NO LINE HERE/) {
    print TYPHOONR1 $_;
  }
}
close(TYPHOON1);
close(TYPHOONR1);

# 격자 분할 및 모델 run
system("cp -a /$FORLD/fort_ROI1.22 /$FORLD/fort.22"); # Fort.22 file 적용
system("$ADCIRC/adcprep --np $PROC --preall");
system("$ADCIRC/adcprep --np $PROC --hotLocalize 67");
system("time mpirun -machinefile ~/mpirun.hosts -np $PROC $ADCIRC/padcirc");
sleep(1);
    
```

fort.15

Early warning simulation modeling for ROI



```

### ADCIRC+SWAN Run(Tide + Typhoon + Wave) ###
unless (open(SWAN1,"<fort_hot_swan_temp.26") { # Fort.26(swan control file) template file open
  stderrMessage("ERROR","Failed to open the fort.26 template file fort_hot_swan_temp.26 for reading.");
  die;
}
unless (open(SWANR1,">SEX_DIR/fort.26") { # 아래의 내용을 적용할 파일
  stderrMessage("ERROR","Failed to open the output control file $SEX_DIR/fort.26.");
  die;
}
while(<SWAN1>) {
  s/%SWAN_START%/SWAN_START/; # SWAN Model Start Time
  s/%SWAN_END%/SWAN_END/; # SWAN Model End Time
  unless (/NO LINE HERE/) {
    print SWANR1 $_;
  }
}
close(SWAN1);
close(SWANR1);
  
```

fort.26

```

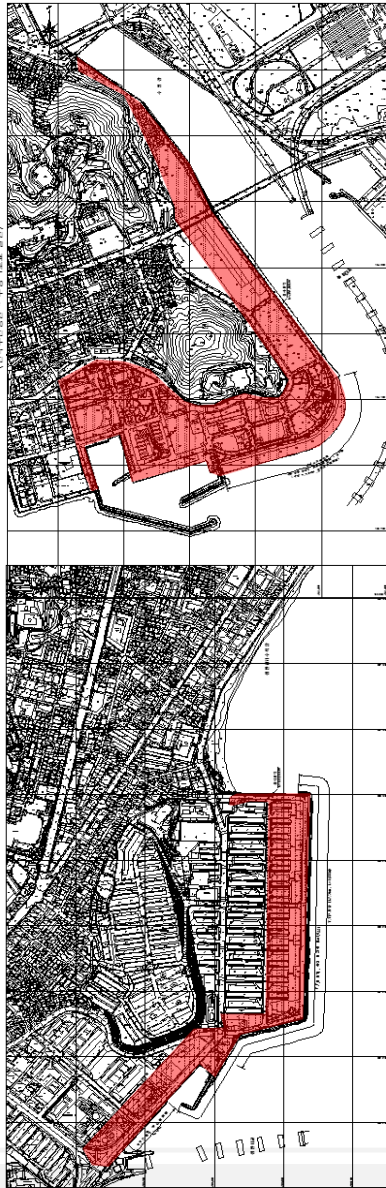
while(<TYPHOON2>) {
  s/%IHOT%/IHOT68/; # hot-start파일 번호
  s/%HRNDAY%/SROI2RNDAY/; # model run time
  s/%NWS%/SNWS_WS/; # 바람강 유선 번호 (NWS=319)
  s/%REFTIME%/SROI1RNDAY/; # model run time
  s/%IREFPR%/SROI1YEAR/; # 바람장 적용시간 (년)
  s/%IREFMO%/SROI1MONTH/; # 바람장 적용시간 (월)
  s/%IREFDAY%/SROI1DAY/; # 바람장 적용시간 (일)
  s/%IREFHHR%/SROI1HOUR/; # 바람장 적용시간 (시)
  s/%StormNumber%/StormNumber/; # 태풍번호
  s/%BLADj%/SBLAdj/; # adjustment factor(at 10 m ==> wind speed)
  s/%RSTIMINC%/SRSTIMINC/;
  # Time increment of input wave radiation stress data from the wave radiation stress forcing file(fort.23) in seconds.
  s/%ROI0HC%/SROI2HC/; # 인계과고
  s/%SLON_DOWN%/SSLON_DOWN/; # ROI2 영역 좌표 (Lon)
  s/%SLAT_DOWN%/SSLAT_DOWN/; # ROI2 영역 좌표 (Lat)
  s/%SLON_UP%/SSLON_UP/; # ROI2 영역 좌표 (Lon)
  s/%SLAT_UP%/SSLAT_UP/; # ROI2 영역 좌표 (Lat)
  s/%HOTSTARTFILE%/SXHNHSTAR/; # hot-start파일생성 간격
  s/%M2NF%/Sm2nf/; # 8분조의 위상 및 진폭 적용
  s/%S2NF%/Ss2nf/;
  s/%N2NF%/Sn2nf/;
  s/%K2NF%/Sk2nf/;
  s/%L1NF%/Sl1nf/;
  s/%O1NF%/So1nf/;
  s/%P1NF%/Sp1nf/;
  s/%Q1NF%/Sq1nf/;
  s/%M2EQARG%/Sm2eqarg/;
  s/%S2EQARG%/Ss2eqarg/;
  s/%N2EQARG%/Sn2eqarg/;
  s/%K2EQARG%/Sk2eqarg/;
  s/%L1EQARG%/Sl1eqarg/;
  s/%O1EQARG%/So1eqarg/;
  s/%P1EQARG%/Sp1eqarg/;
  s/%Q1EQARG%/Sq1eqarg/;
  unless (/NO LINE HERE/) {
    print TYPHOONR2 $_;
  }
}
close(TYPHOON2);
close(TYPHOONR2);

system("cp -a /SNFORLD/fort_ROI2 re.2 /SNFORLD/fort.22"); # 태풍 중심위치가 위도 25도 이상인 fort.22파일 적용
system("cp -a /SNFORLD/FE0000/fort.68 /SNFORLD/fort.68"); # hot-start파일 적용
sleep 1);
# 격자 분할 및 모델 run
system("$ADCIRC/adcprep --np $PROC --preall");
system("$ADCIRC/adcprep --np $PROC --hotLocalize 68");
system("time mpirun -machinefile ~/mpd12z.hosts -np $PROC $ADCIRC/padcswan");
sleep 1);
  
```

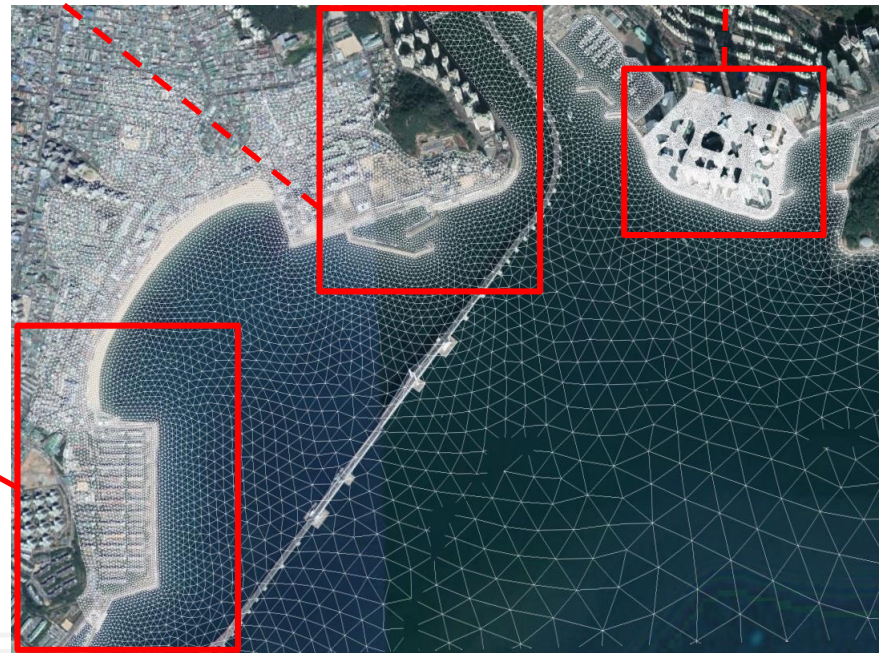
fort.15

Storm wave inundation records

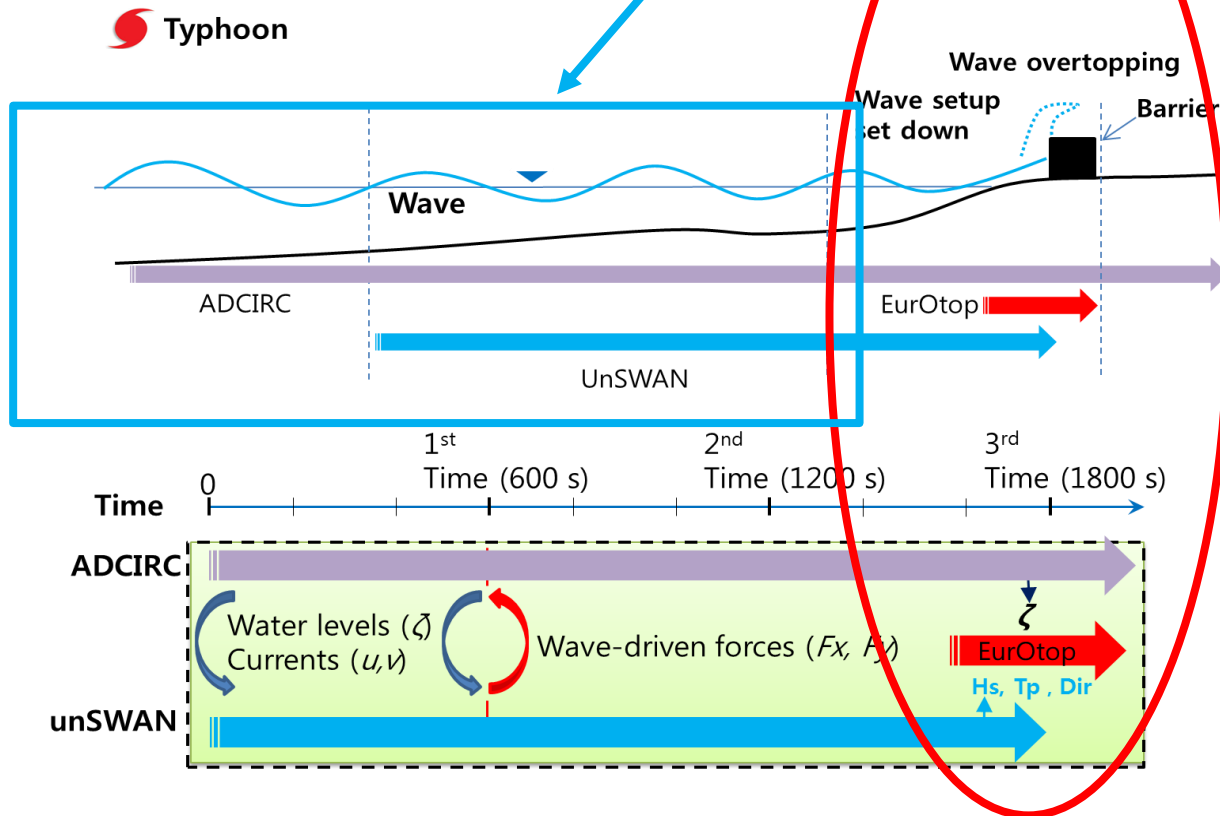
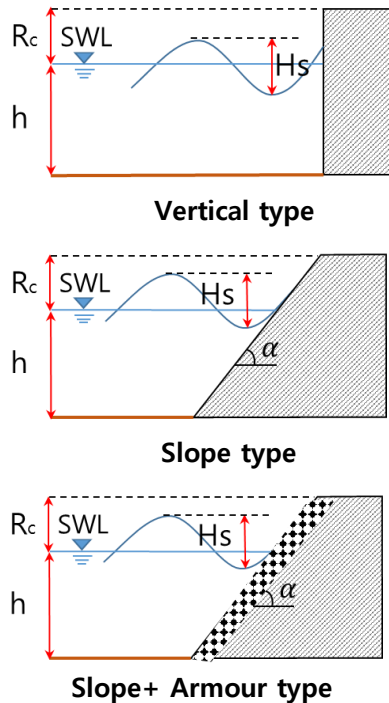
Maemi (TY0314)



Chaba (TY1618)

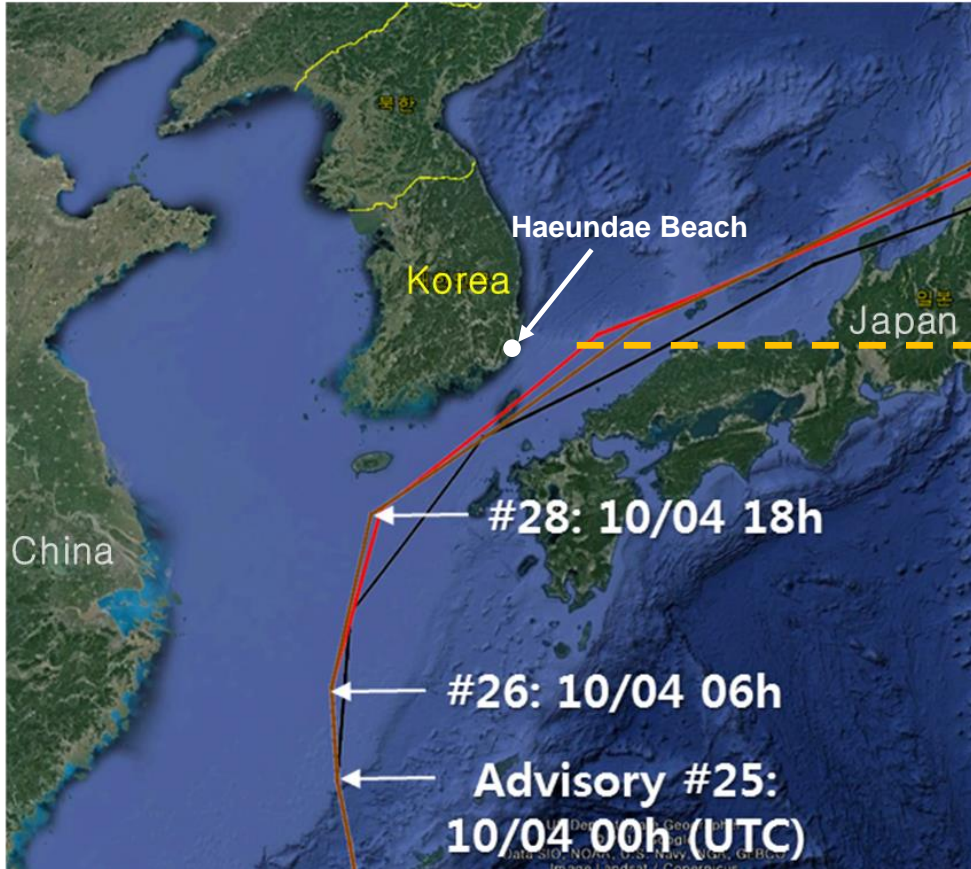


▪ EurOtop coupling (embedding empirical eq. into storm surge model)



Typhoon tracks and characteristics

Tracks of Typhoon Chaba (2016) wrt advisories



Typhoon path

Typhoon Chaba (Igme)

Typhoon (JMA scale)

Category 5 (Saffir–Simpson scale)



Typhoon Chaba at peak intensity on October 3, observed from the [International Space Station](#)

Formed	September 24, 2016
Dissipated	October 7, 2016 (Extratropical after October 5)
Highest winds	<i>10-minute sustained:</i> 215 km/h (130 mph) <i>1-minute sustained:</i> 270 km/h (165 mph)
Lowest pressure	905 hPa (mbar); 26.72 inHg
Fatalities	7
Damage	\$18.3 million (2016 USD)
Areas affected	South Korea, Japan
Part of the 2016 Pacific typhoon season	

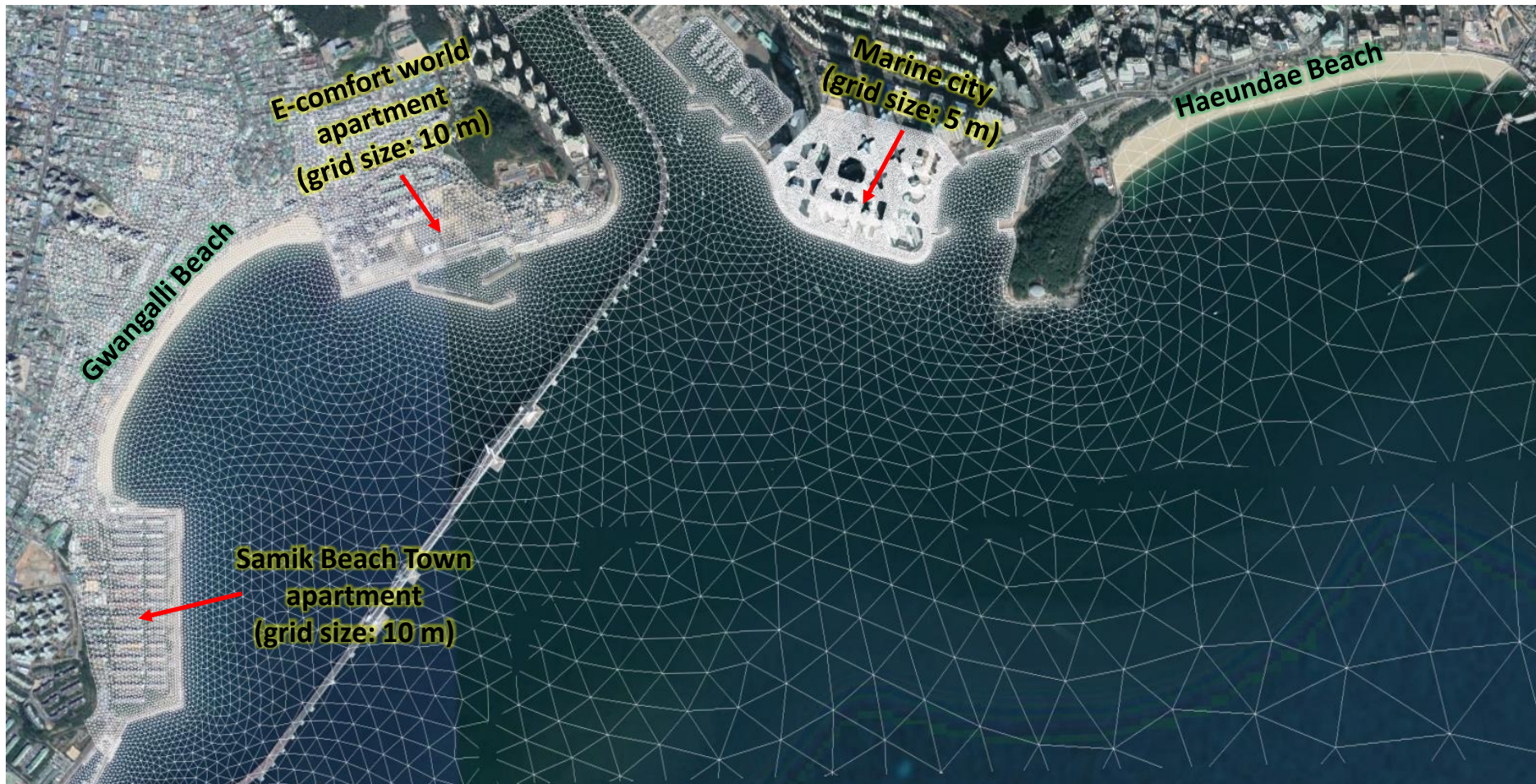
Latitude (degree)

00

en.wikipedia.org

Patching grids to base storm surge model

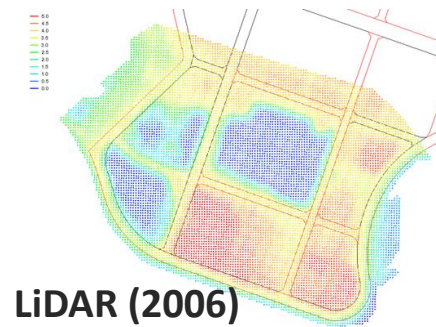
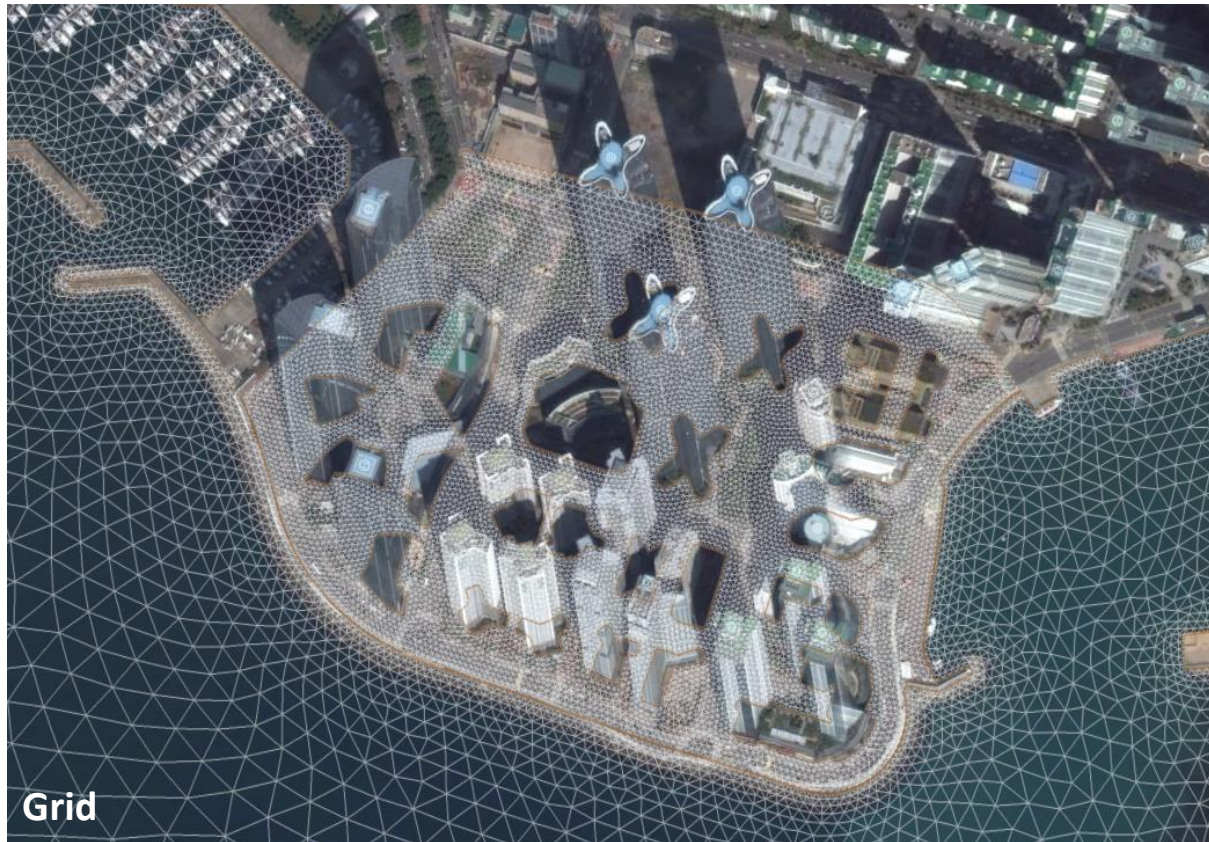
- ✓ Based on NWP-116k grid
- ✓ Applied fine bathymetry data, GTOPO30 & KorBathy30s
- ✓ # of Nodes : 144,079, dt : 0.1 sec, simulation: 3.5 days, (took ~ 2 h by 180 cores)



Gridding for marine city modeling

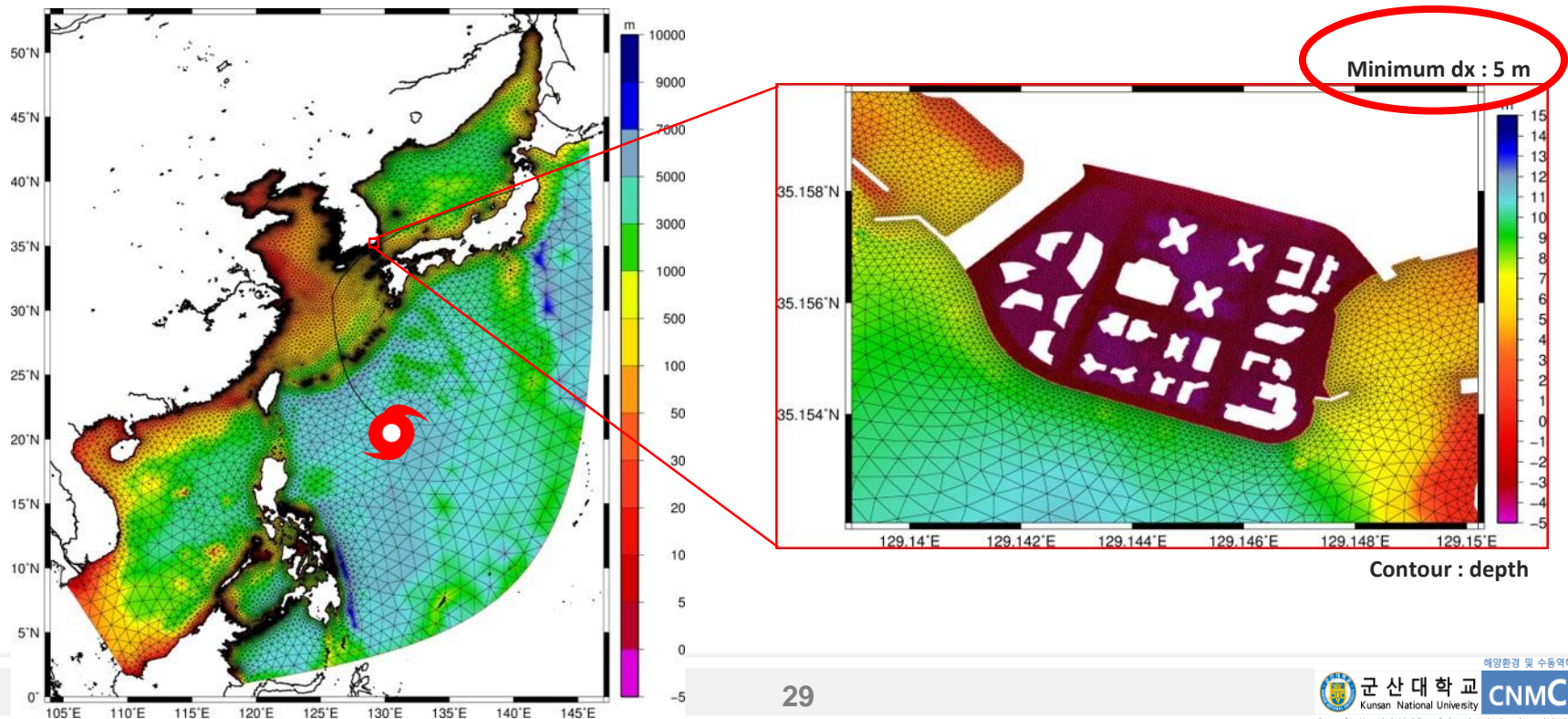
Overland grids by using topography data

- ✓ LiDAR by National Geographic Information Institute & DEM of 1:1000
- ✓ Local government data of Haeundae-gu Office in 2012



Wave overtopping modeling

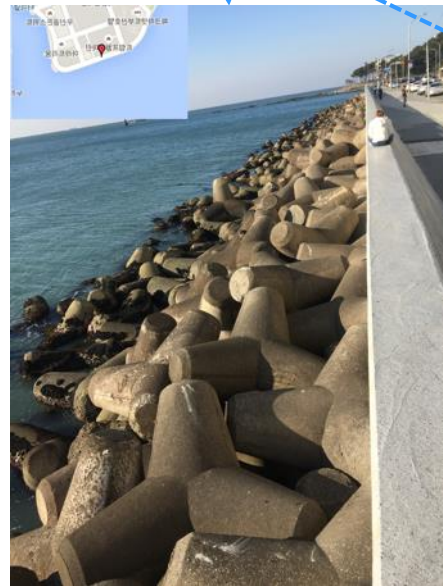
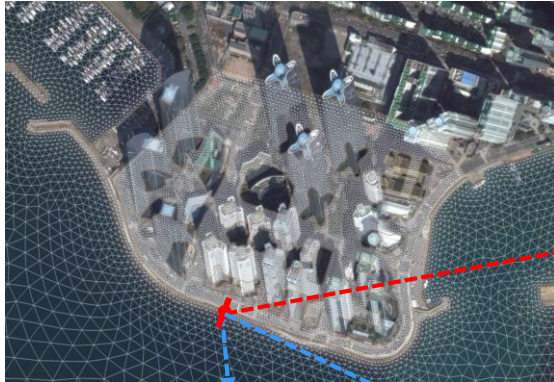
- ✓ Based on NWP-116k grid
- ✓ Applied fine bathymetry data, GTOPO30 & KorBathy30s
- ✓ ADCIRC+SWAN and considering dynamic asymmetric wind for Typhoon Chaba
(Peak Pc: 905 hPa, MWS: 60 m/s)
- ✓ # of Nodes : 132,657, dt : 0.1 sec, simulation: 10.75 days, (took ~ 6 h by 120 cores)



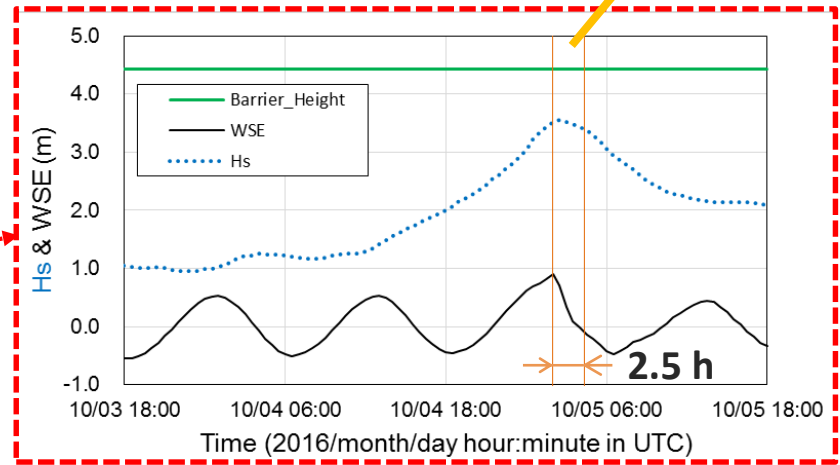
Marine city wave overtopping simulation

Dimension of barrier

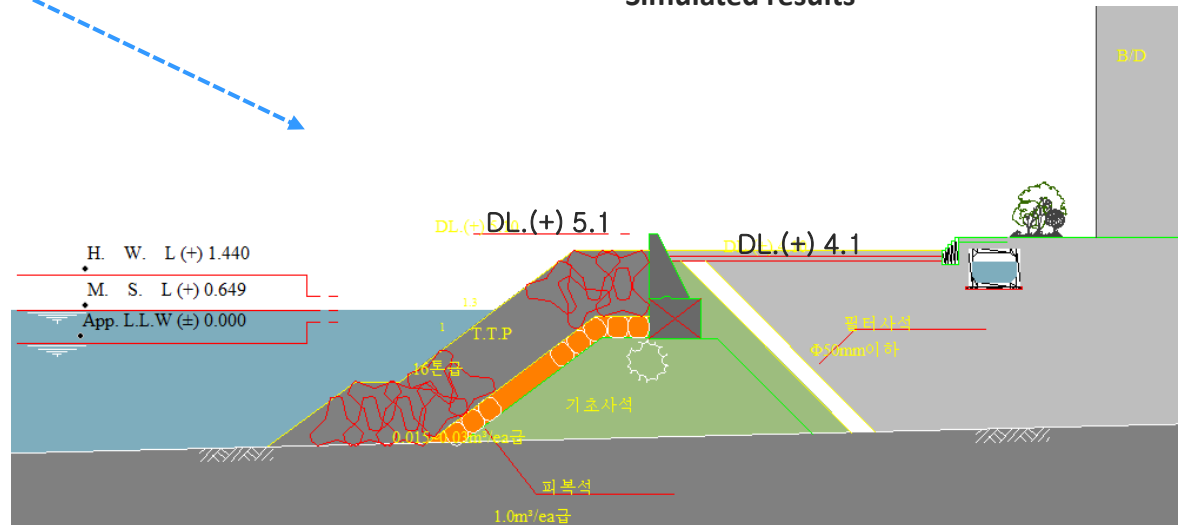
- ✓ Parapet crest: 4.42 m, Max. WSE : 0.94 m, Max. significant wave height: 3.55 m



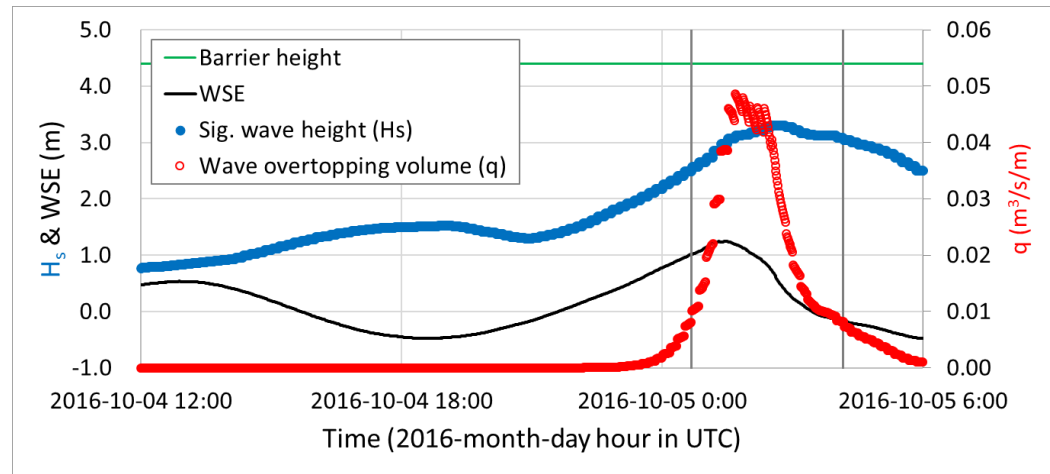
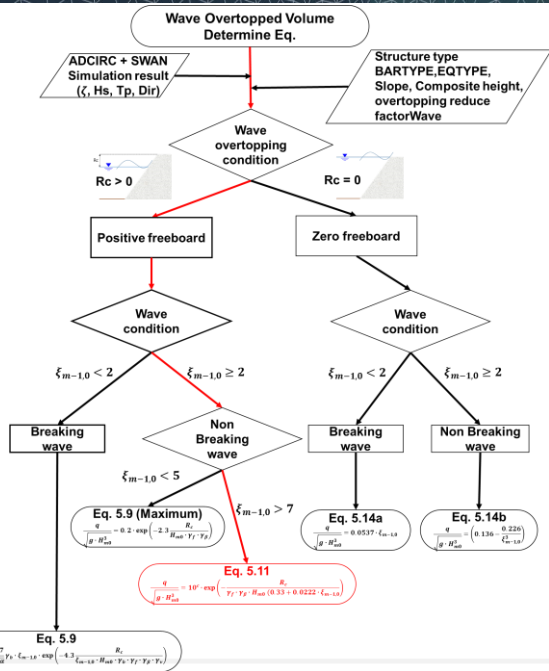
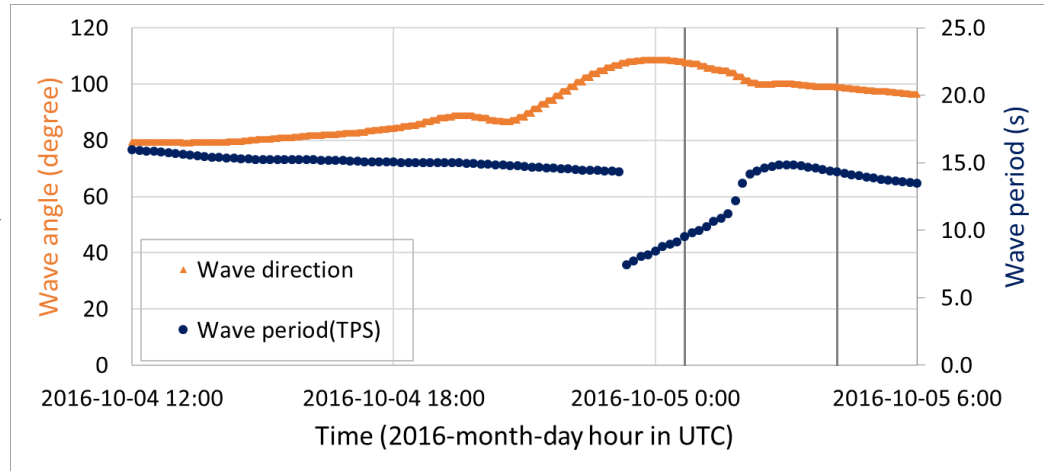
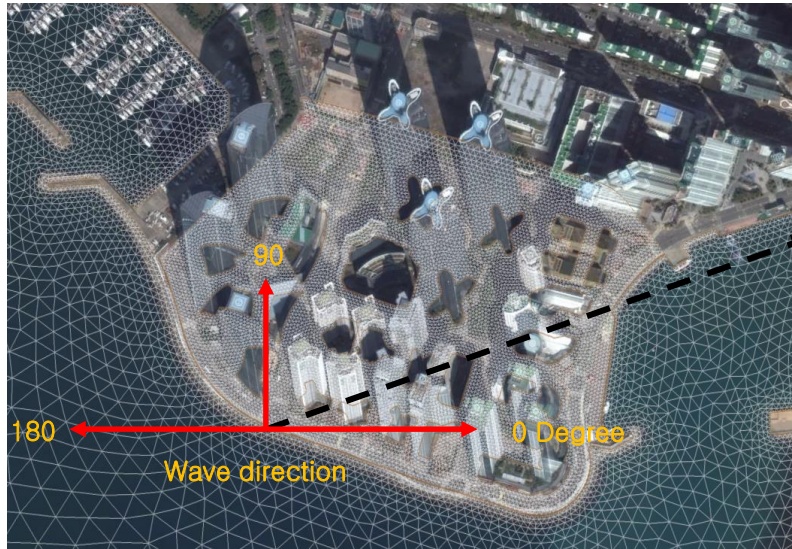
Wave overtopping
(10/05 02:00 ~ 10/05 04:30)



Simulated results



Analysis of incoming wave characteristics and WOT

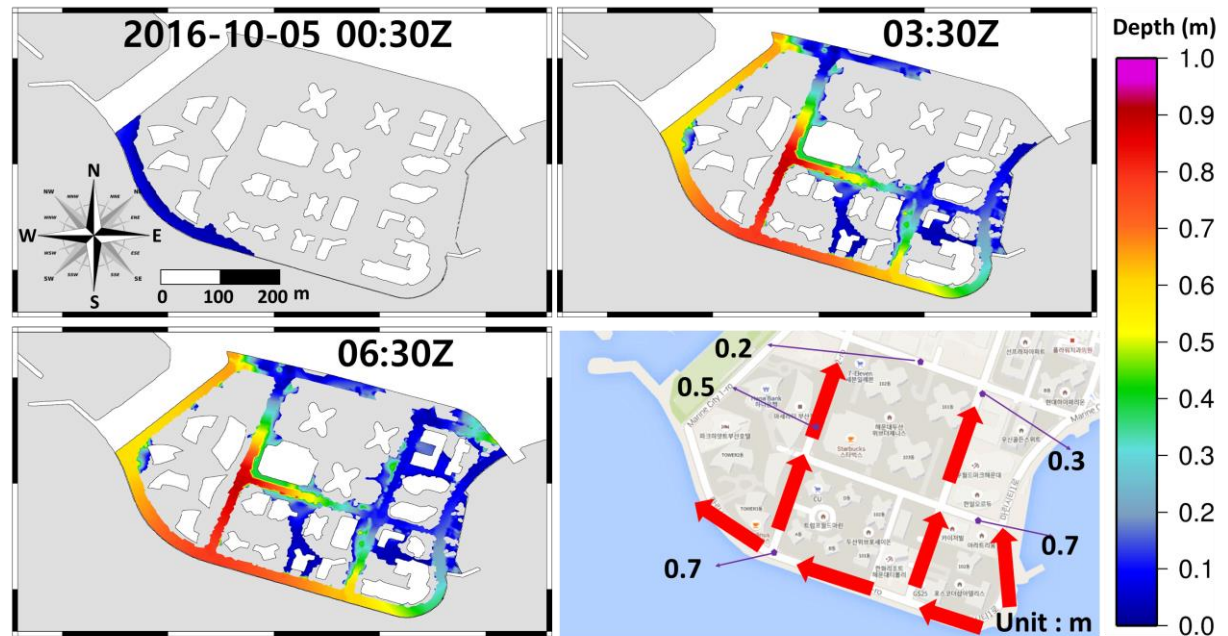


Wave overtopping and propagation of inundation

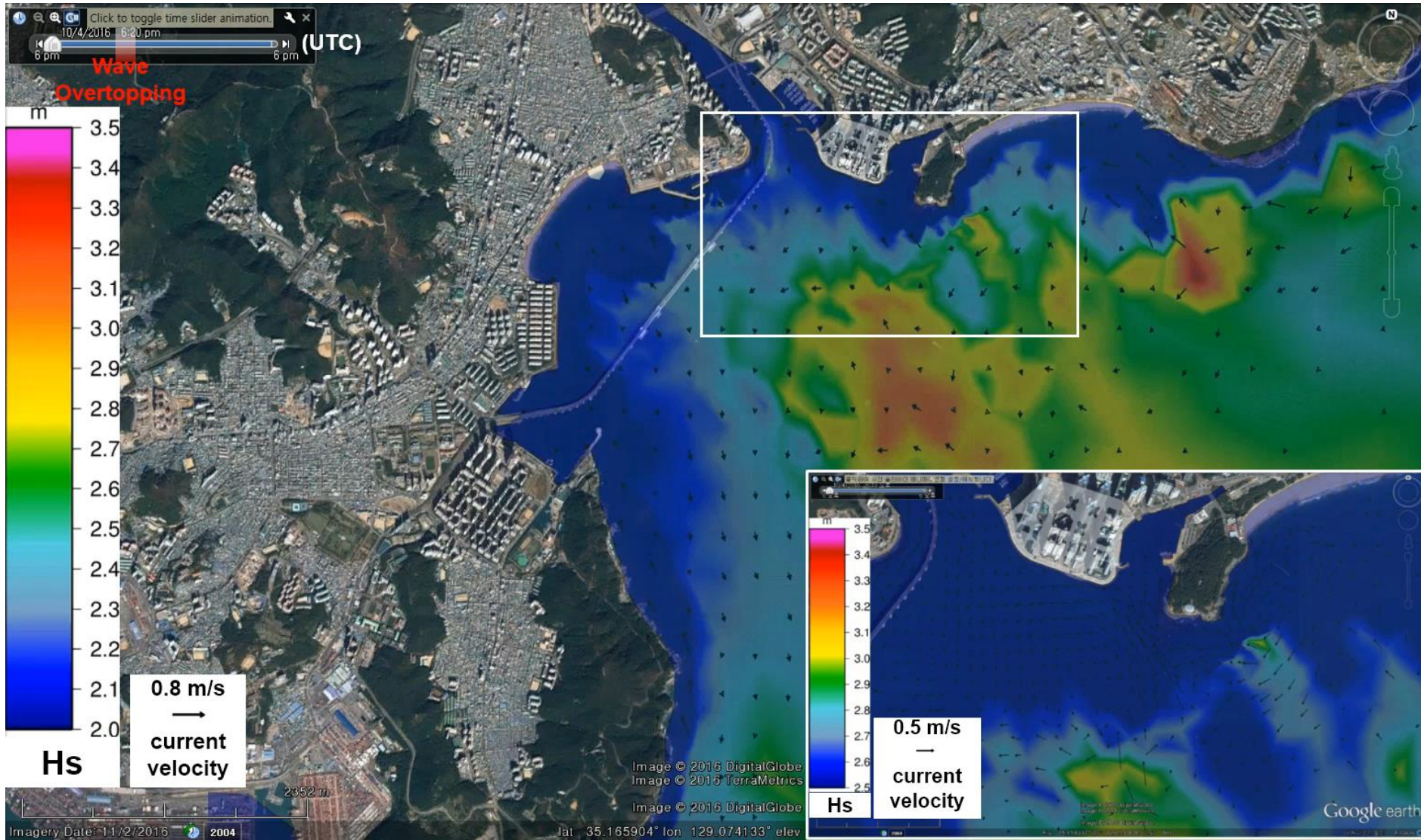


Wave dir. & periods

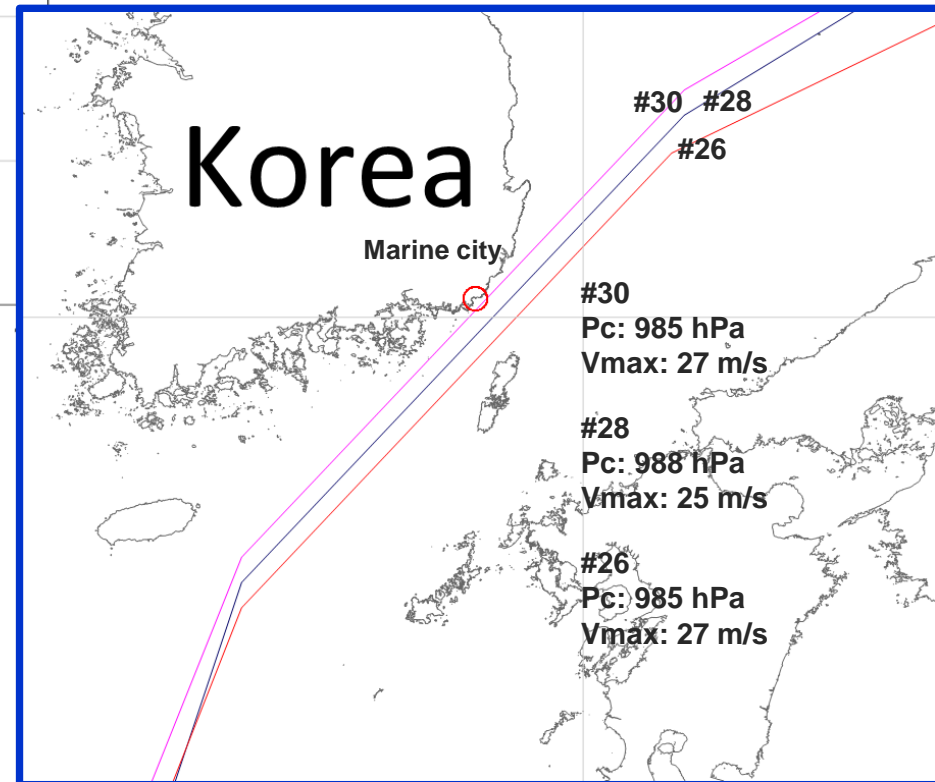
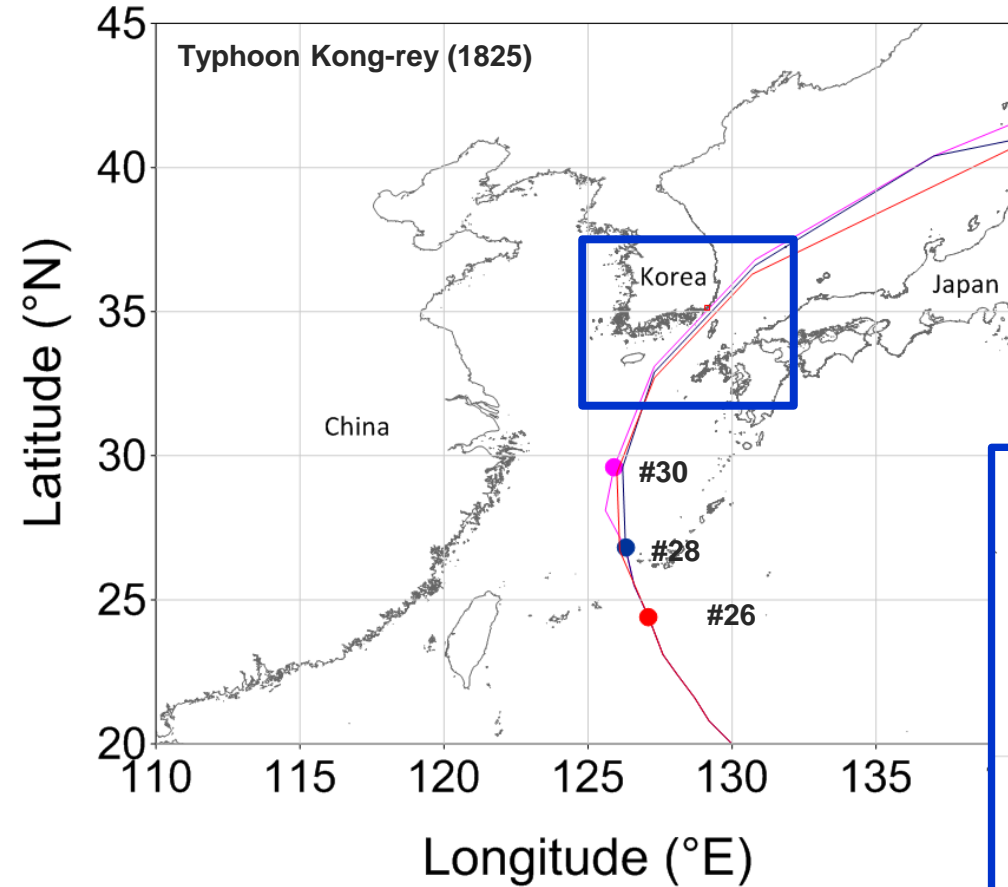
Propagation of overland inundation due to WOT



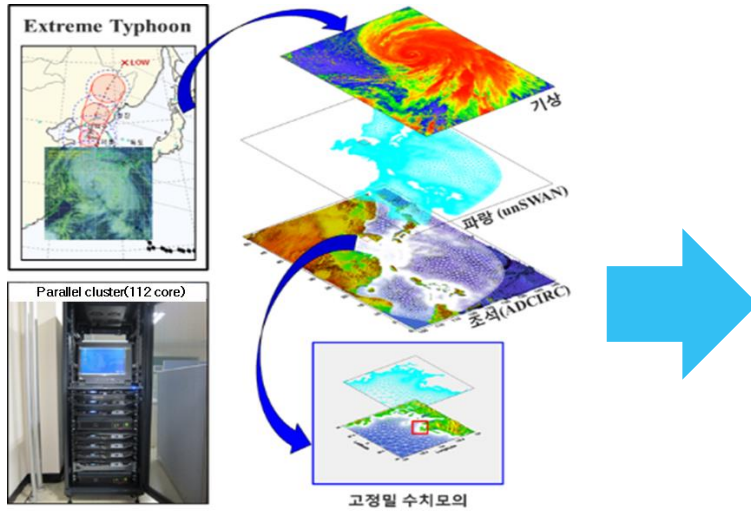
Marine city wave overtopping animation



EWS of WOT in 2018 induced by typhoon Kong-rey



Based on a real-time surge forecasting



youtube.com/watch?v=PPH0rZA_uw

일요일, 10 11월 2019

해양환경 및 수동역학 모델링 연구실

Center for Numerical Modeling of Coastal Hydrodynamics and Environmental Transport

해양환경 및 수동역학 모델링 연구실

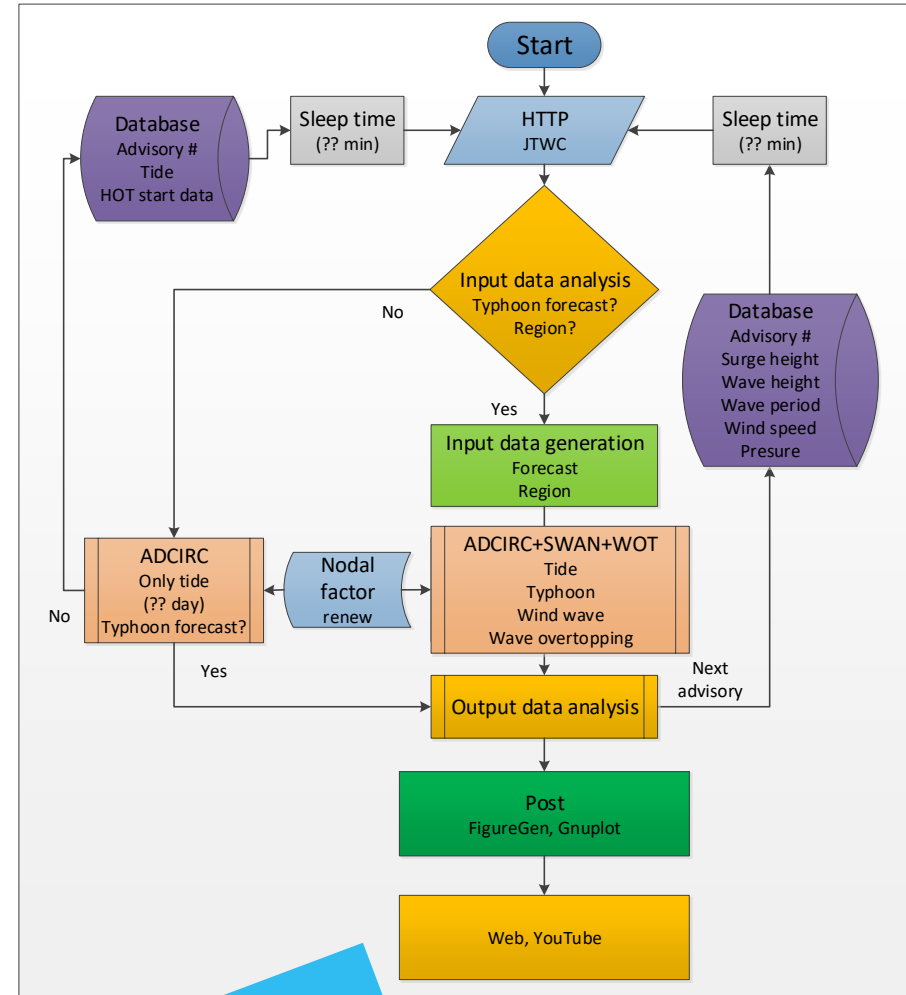
태풍 미탁 내습에 따른 해일고 예측

Forecasting of storm surge elevation induced by typhoon : MITAG

Update time : 2019. 10. 02. 10:00 KST

지역명	최대해일고 (m)	발생시간 (KST)	최대해일속 (cm/s)	발생시간 (KST)
간성	2.86	19-10-1 6:00	0.40	19-10-2 16:00
홍성	1.91	19-10-1 4:00	0.37	19-10-2 9:00
한포	1.97	19-10-2 23:00	0.36	19-10-2 20:00
사천	0.96	19-10-1 2:00	0.34	19-10-2 2:00
서해	2.52	19-10-1 20:00	0.31	19-10-2 24:00
홍성	1.40	19-10-2 23:00	0.40	19-10-2 21:00
서해	0.97	19-10-2 20:00	0.32	19-10-2 23:00

YouTube video player showing a map of surge elevation and a graph of surge elevation over time.



Comparison of WOT wrt precedent typhoon advisories

